AMENDMENTS TO THE SPECIFICATION

Please Amend the Specification as indicated below. Additions are indicated by instructions or underlining and deletions by strikethroughs.

On page 1, before the paragraph starting on line 8, please Insert on a separate line --BACKGROUND--.

On page 3, before the paragraph starting on line 1, please Insert on a separate line --SUMMARY--.

On page 7, please Replace the paragraph starting on line 1 with:

According to a particularly advantageous embodiment, in which the guiding of the element that forms an interference or baffle region, in particular the baffle plate, can take place independently from the implementation of the hydrodynamic clutch, in particular of the blade carrying parts and on other components according to c) and d), is characterized by that the respective impeller, viewed in cross section, is in the radial direction correspondingly turned away. ~~[Tr.- this is translated literally but does not make sense, the original here is, I believe, incorrect - what is probably meant is:" A particular..." (that is, with "According to" omitted.)].~~ A ring-shaped element is thereby abraded with respect to the blading either in the region of the external circumference or in the region of the internal circumference, whereby the blading, viewed in cross section, is characterized by blade sides and/or blade ends that are constructed in radial direction parallel to the rotation axis. This means that the ring-shaped turning-away extends over the total axial extension of the respective impeller or at least a part of the region of certain magnitude which corresponds at least to the sum of the displacement and the width of the baffle plate. The baffle plate can then be displaced in the region of the parting plane over the total extension and even beyond it relative to the respective impeller, whereby the baffle plate can be supported also by a stationary element or an element which rotates with a relative rotation speed with respect to the respective impeller, and which can be guided on it displaceable in the axial direction.

On page 11, before the paragraph starting on line 10, please Insert on a separate line --BRIEF DESCRIPTION OF THE DRAWINGS--.

On page 12, before the paragraph starting on line 8, please Insert on a separate line --DETAILED DESCRIPTION--.

On pages 14-15, please Replace the paragraph starting on page 14, line 8 with:
Contrary to this, figures 2a and 2b demonstrate with the aid of two views an alternative arrangement of an implementation of a hydrodynamic clutch 1.2 with an axially displaceable baffle plate 5.2. The latter is constructed in this case as a separate component and displaceable in the axial direction opposite the impeller, here, for example, the primary impeller 2.2, in such a sway that a change of the active surface in the working chamber 4.2 arises through the displacement. The baffle plate 5.2 is in this case also constructed as an external baffle 6.2. That is, it is arranged in the external region of the working chamber 4.2 and is supported in it. The flow is thereby reversed in this region around the baffle and/or the baffle plate 5.2 before it overflows into the secondary impeller ~~3~~3.2. In this implementation the blades 14.2 are arranged in such a way that they project into the radial external region of the primary impeller 2.2 over the blade carrying part 8.2, i.e., they are guided only over a part of their extension in the radial direction at the blade carrying part 8.2 and that the radial external region of the primary impeller 2.2 is free from the in figure 1 represented wall region 7.2. The baffle plate 5.2 is in this case constructed with slits and is guided at the individual blades 14.2 that are arranged in the circumferential direction at a distance to each other. These are preferably directed straight, i.e., the individual blade 14.2 in arranged in a plane which is characterized by a vertical theoretical rotation axis and the rotation axis. The axially displaceable baffle plate 5.2 is thereby guided in a region of the blade 14.2, here in particular a freely projecting blade region 13.2, which is free from a direct guidance on the blade carrying part 8.2 and is fixated in its position only by the other baffle regions in the blade carrying part 8.2. Implementations with slanted blading are likewise conceivable but then the guiding slits are to be designed with a corresponding width or the axial

displacement is to be secured by twisting in the circumferential direction. According to the magnitude of the blade region 13.2 and/or the blade carrying part 8.2, the displacement in an axial direction can be guaranteed by individual guidance of the baffle plate 5.2 on the blading 14.2. An optimal displacement of the baffle plate 5.2 can be achieved in the case that the end region of the blading carrying region 8.2 lies in a plane that is perpendicular to a plane that is characterized by a perpendicular to the rotation axis and a perpendicular in the vertical direction and/or extends parallel to the parting plane T between the primary impeller 2.2 and secondary impeller 3.2. According to the arrangement of its internal diameter $d_{i5.2}$ this can take place either up to the region outside the impeller, here the primary impeller 2.2, or at least up to the region of the blade carrying part 8.2. If in the represented case the internal diameter $d_{i5.2}$ is equal or preferably larger than the external diameter d_{A8} of the blade carrying part 8.2, then a concise displacement to the blade carrying part 8.2 can take place in the axial direction or even completely over the blade carrying part 8.2 out of the working chamber 4.2. However, this is not aimed at since then it is no longer possible to guide the baffle plate 5.2 without additional accessories. Preferably, implementations are thereby aimed at in which a displacement takes place as far as possible in the direction of the blade carrying part 8.2 and/or the inner wall ~~15~~ that is formed by it. A concise termination and/or a stop function of the blade carrying part 8.2 is preferably aimed at.

On page 19, please Replace the paragraph starting on line 13 with:

As an example, figure 7 demonstrates with the aid of a ny(v)~~γ~~-λ-diagram ~~[Tr. the 'γ' character is written in by hand in the original and is not very clear]~~ the operation mode of the element 5, which forms the interference and baffle region, plotted in different positions over the rotational speed ratio. This shows that precisely in the startup region, i.e., at very high slippage, in relation to the known implementations from the state of the art, substantially smaller torques are picked-up because of the action of the baffle plate 5 in the region of the parting plane T. At very low slippage, i.e., a thereto proportional rotational speed ratio ny(v) ~~γ [Tr. here also, I assume it is 'γ']~~ in the range of 1 during the ensuing displacement of the baffle plate 5 still outside the working chamber and/or in a position in which it does no longer affects an interference of the circulation flow, the effect of the baffle plate is not detectable.

On page 20, please Replace all the text on the page with:

Symbol Reference List

1, 1.2,1.3a, 1.3b, 1.3c, 1.4a, 1.4b	hydrodynamic clutch
2, 2.2, 2.3a 2.3b, 2.3c, 2.4, 2.4a, 2.4b	primary impeller
3, 3.2, 3.3a, 3.3b, 3.3c, 3.4, 3.4a, 3.4b	secondary impeller
4,4.2,4.3a, 4.3b, 4.3c, 4.4, 4.4a, 4.4b	working chamber
5, 5.2, 5.3a 5.3b, 5.3c, 5.4a 5.4b, 5.5	baffle plate
6, 6.2, 6.3a	external baffle
7,7.2	wall region
8,8.2	blade carrying part
9	front surface
10	front surface
11	front side
12	front side
13	blade region
14	Blade
~~15~~	~~inner wall~~
16	slit
17.3b,17.3c	internal baffle
18	slit
19	core chamber
20	active and/or influencing surface
21	casing